

BOILER REPLACEMENT GUIDE

Step-by-step procedures for properly sizing hot water and steam replacement boilers for homes and small commercial buildings



BOILER REPLACEMENT GUIDE

INTRODUCTION

This booklet is designed to give the qualityconscious hydronic heating contractor a stepby-step procedure for properly sizing hot water and steam replacement boilers. It is intended primarily for use in sizing boilers for homes, but in many cases can also be used for small commercial buildings.

All too often replacement boilers are sized simply by matching the rating of the old boiler. This can result in an oversized boiler which wastes fuel—or an undersized unit which will not heat the building.

By following the procedures in this booklet, the heating contractor will be able to accurately size replacement boilers, sell more replacement jobs, assure energy-efficient installations, and render better service for customers.

SIZING HOT WATER BOILERS - Page 3

There is only one accepted method for determining the proper size of a replacement hot water boiler: THE HEAT LOSS OF THE BUILDING MUST BE CALCULATED. By following the steps in this booklet, the total heat loss of the average house can be calculated in five or ten minutes. In most cases it should not be necessary to make a detailed calculation but, if it is required for any reason, use or the latest ASHRAE Handbook.

SIZING STEAM BOILERS - Page 9

To properly size a replacement steam boiler DETERMINE THE TOTAL BTU CAPACITY OF THE CONNECTED RADIATION. This method is necessary in order to assure adequate steam pressure to fill all parts of the system.

INDEX TO FIGURES & TABLES

| | | PAGE | | | PAGE |
|----------|--|------|----------|--|------|
| Figure 1 | Job Survey Form | 3 | Figure 3 | Material List | 7 |
| Figure 2 | Heat Loss Calculation Form | 4 | Figure 4 | Job Survey Form-Example | 8 |
| Table A | Construction Characteristics | 4 | Figure 5 | Heat Loss Calculation Form- Example | 9 |
| Table B | Heat Loss Table | 5 | Figure 6 | Radiator Styles | 9 |
| Table C | Design Temperature Correction Factors | 6 | Figure 7 | Radiator Example | 10 |
| Table D | Ceiling Correction Factors | 6 | Table F | Radiator Ratings | 10 |
| Table E | Net Ratings of Weil-McLain Boilers | 7 | | | |

SECTION 1 PROCEDURE FOR SIZING HOT WATER BOILERS

STEP 1: COMPLETE A JOB SURVEY FORM

Certain key information is required for each boiler replacement job in order to calculate the heat loss, select the proper boiler and determine the selling price. Figure 1 is a Job Survey Form (part of a Weil-McLain Boiler Replacement Worksheet) to aid in recording the required information. It will serve as a checklist of the basic data for the existing installation and a permanent record for your job file. Boiler Replacement Worksheets to be used with this booklet are available through Weil-McLain distributors and sales representatives.

FIGURE 1: JOB SURVEY FORM

| | | WEIL | ·McLA | IN ® | |
|------------------------|----------------|-----------|--------------------|-------------|-----------|
| ВО | ILER REP | | IENT WO | ORKSHE | ET |
| CUSTOMER NAME: | - | | | PHON | E: |
| ADDRESS: | | | | | |
| PREPARED BY: | | | | | |
| PRESENT HEATING SY | 'STEM: | | | | |
| TYPE OF RADIATION: _ | | | | | |
| HEATING MEDIUM: | □ Hot Water | | | | |
| FUEL NOW USED: | | - | | - | |
| FUEL TO BE USED: | | • | | Electricity | |
| IS SYSTEM HEATING S | | | | | |
| If no, what is the pro | | | | | |
| How can it be correc | | | | | |
| RELOCATE BOILER? | | No lf ye | es estimate time _ | M | laterials |
| Corrosive Atmosphe | | | | | |
| PRESENT SOURCE OF | | | | | |
| WILL NEW BOILER HAV | | R? □Yes | □ No Type | | |
| HOUSE CONSTRUCTIO | | | | | |
| GLASS: | | | | | |
| WALLS: | | | | | |
| | | | | | |
| SLAB: | | | | | |
| HOUSE DIMENSIONS (| • | • / | | | |
| High Altitude | | | | | |
| Basement | ' H x ' H x | | | • | |
| | | | | • | |
| | | | | 5q. ft. | |
| | | | | | |
| NEW THERMOSTAT(S) | | tandard L | Programmable | | |

STEP 2: CALCULATE TOTAL HEAT LOSS

The form shown in Figure 2 (Part of the Weil-McLain Boiler Replacement Worksheet) can be used for calculating total heat loss by following these steps.

- Based on the type of construction, amount of insulation, etc., select the Construction Design Number from Table A below which most nearly matches each of the areas (levels) to be heated.
- 2. Determine the total square footage of each area to be heated from the Job Survey Form. Round to the nearest hundred.
- 3. Based on the Construction Design Number selected and the square footage of each area, determine the heat loss (at 70°F design temp. diff.) from Table B (page 5). NOTE: Do not add

in heat loss for basements which are not to be heated; ignore crawl spaces which are open to basement areas.

- 4. If the Outdoor Design Temperature of the city is unknown, refer to back page. If the design temperature difference is other than 70°F, multiply the heat loss for each area by the appropriate correction factor from Table C (page 6). Round to the nearest ten.
- 5. If it is a two story house, multiply the heat loss of the first level by the appropriate Ceiling Correction Factor from Table D (page 6). Round to nearest ten.
- 6. Add the adjusted heat loss for each area to determine the Total Heat Loss.

| LEVEL | CONSTRUCTION NUMBER | SQ. FT. | HEAT LOSS (AT 70°F DESIGN TEMP. DIFF.) | CORRECTION FACTOR AT | TOTAL | CEILING CORRECTION FACTOR | ADJUSTED HEAT LOSS |
|--------------|------------------------|---------|---|-------------------------|-------|---------------------------------|-----------------------|
| FIRST LEVEL | | | x | = | x | = | |
| SECOND LEVEL | | | | = | | > | |
| BASEMENT | | | ^ ^ X | | | | |
| SLAB | | | | | | | |
| | | | · ^ | | тот | AL HEAT LOSS | |

FIGURE 2: HEAT LOSS CALCULATION FORM

TABLE A: CONSTRUCTION CHARACTERISTICS

| | FRAME CONST | RUCTION | BRICK CONSTRUCTION | | | |
|-------------------------------|--------------------------|---------------------|----------------------|-------------------------------|--|-----------------------|
| | WEATHERSTRIPPED GLASS | INSULATION WALL | THICKNESS CEILING | | WEATHERSTRIPPED GLASS | CEILING INSULATION |
| CONSTRUCTION DESIGN NUMBER | Without | basement or crawl s | pace | CONSTRUCTION DESIGN NUMBER | With 4" brick & 4" lig | htweight block** |
| 1 | single | 1″ | 2" | 14 | single | 2" |
| 2 | double | 1″ | 2" | 15 | double | 2″ |
| 3 | single | 1″ | 3" | 16 | single | 3″ |
| 4 | double | 1″ | 3" | 17 | double | 3″ |
| 5 | double | 2" | 3" | | With 8" bi | rick** |
| 6 | double | 3" | 3" | 18 | single | 2″ |
| | With full | basement or crawl s | space | 19 | double | 2″ |
| 7 | double | 3" | 6″* | 20 | single | 3″ |
| 8 | double | 3" | 6″ | 21 | double | 3″ |
| 9 | double | 3" | 9″ | | For Basements- Concrete or block walls 8' high, 6 1/2' below grade (stray heat from boiler & piping included). Or for unheated crawl spaces | |
| 10 | double | 3″ | 12″ | 22† | | |
| 11 | double | 6″ | 6″ | | | |
| 12 | double | 6″ | 9″ | 23‡ | 4" concrete slab with 1" perimeter insulation | |
| 13 | double | 6″ | 12″ | 254 | | |

* With 2" Floor Insulation.

** Furred, lath & plaster.

⁺ Use for basement heat losses WITHOUT fully exposed walls and for floor losses over closed unheated crawl spaces.

For basements with fully exposed walls use FIRST FLOOR heat loss.

‡ Use for grade level slab construction.

TABLE B: HEAT LOSS TABLE (in BTU/Hr.) (Calculated at 70°F Design Temperature Difference

| FLOOR | | | | C | ONSTRUC | | GN NUMBE | R | | | |
|-----------------|--------|--------|--------|--------|---------|--------|----------|--------|--------|--------|--------|
| AREA SQ. FT. | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
| 500 | 28,750 | 23,900 | 27,350 | 22,510 | 18,080 | 16,860 | 17,910 | 16,160 | 15,460 | 15,110 | 15,360 |
| 600 | 32,300 | 27,030 | 30,620 | 25,350 | 20,520 | 19,200 | 20,460 | 18,360 | 17,520 | 17,100 | 17,490 |
| 700 | 35,860 | 30,150 | 33,900 | 28,190 | 22,970 | 21,540 | 23,010 | 20,560 | 19,580 | 19,090 | 19,610 |
| 800 | 39,840 | 33,590 | 37,600 | 31,350 | 25,640 | 24,080 | 25,760 | 22,960 | 21,840 | 21,280 | 21,920 |
| 900 | 43,340 | 36,680 | 40,820 | 34,160 | 28,050 | 26,380 | 28,270 | 25,120 | 23,860 | 23,230 | 24,010 |
| 1000 | 46,890 | 39,800 | 44,090 | 37,000 | 30,500 | 28,720 | 30,820 | 27,320 | 25,920 | 25,220 | 26,140 |
| 1100 | 50,450 | 42,920 | 47,370 | 39,840 | 32,940 | 31,060 | 33,370 | 29,520 | 27,980 | 27,210 | 28,270 |
| 1200 | 54,000 | 46,040 | 50,640 | 42,680 | 35,390 | 33,400 | 35,920 | 31,720 | 30,040 | 29,200 | 30,400 |
| 1300 | 56,640 | 48,470 | 53,000 | 44,830 | 37,340 | 35,300 | 38,030 | 33,480 | 31,660 | 30,750 | 32,120 |
| 1400 | 60,200 | 51,590 | 56,280 | 47,670 | 39,790 | 37,640 | 40,580 | 35,680 | 33,720 | 32,740 | 34,240 |
| 1500 | 62,830 | 54,030 | 58,630 | 49,830 | 41,740 | 39,540 | 42,690 | 37,440 | 35,340 | 34,290 | 35,970 |
| 1600 | 65,530 | 56,490 | 61,050 | 52,010 | 43,730 | 41,480 | 44,840 | 39,240 | 37,000 | 35,880 | 37,730 |
| 1700 | 68,590 | 59,250 | 63,830 | 54,490 | 45,910 | 43,570 | 47,140 | 41,190 | 38,810 | 37,620 | 39,630 |
| 1800 | 71,720 | 62,040 | 66,680 | 57,000 | 48,130 | 45,710 | 49,490 | 43,190 | 40,670 | 38,410 | 37,950 |
| 1900 | 73,930 | 64,150 | 68,600 | 58,830 | 49,860 | 47,410 | 51,400 | 44,750 | 42,090 | 40,760 | 43,120 |
| 2000 | 77,050 | 66,940 | 71,450 | 61,340 | 52,080 | 49,550 | 53,750 | 46,750 | 43,950 | 42,550 | 45,070 |

TABLE B (continued)

| FLOOR | | CONSTRUCTION DESIGN NUMBER | | | | | | | | | | |
|-----------------|--------|----------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| AREA SQ. FT. | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
| 500 | 14,660 | 14,310 | 30,360 | 25,520 | 28,960 | 24,120 | 32,780 | 27,940 | 31,380 | 26,540 | 5,130 | 4,350 |
| 600 | 16,650 | 16,230 | 34,060 | 28,790 | 32,380 | 27,110 | 36,690 | 31,420 | 35,010 | 29,740 | 6,150 | 4,730 |
| 700 | 18,630 | 18,140 | 37,760 | 32,050 | 35,780 | 30,090 | 40,600 | 34,890 | 38,650 | 32,930 | 7,180 | 5,220 |
| 800 | 20,800 | 20,240 | 41,920 | 35,670 | 39,680 | 33,430 | 45,040 | 38,790 | 42,800 | 36,550 | 8,210 | 5,600 |
| 900 | 22,750 | 22,120 | 45,560 | 38,910 | 43,040 | 36,390 | 48,890 | 42,240 | 46,370 | 39,720 | 9,230 | 5,980 |
| 1000 | 24,740 | 24,040 | 49,260 | 42,170 | 46,460 | 39,370 | 52,810 | 45,720 | 50,010 | 42,920 | 10,250 | 6,370 |
| 1100 | 26,730 | 25,960 | 52,960 | 45,430 | 49,880 | 42,350 | 56,720 | 49,190 | 53,640 | 46,110 | 11,300 | 6,750 |
| 1200 | 28,720 | 27,880 | 56,660 | 48,690 | 53,300 | 45,330 | 60,630 | 52,670 | 57,270 | 49,310 | 12,330 | 7,150 |
| 1300 | 30,300 | 29,390 | 59,360 | 51,200 | 55,720 | 47,560 | 63,450 | 55,290 | 59,810 | 51,650 | 13,340 | 7,330 |
| 1400 | 32,280 | 31,300 | 63,060 | 54,460 | 59,140 | 50,540 | 67,360 | 58,760 | 63,440 | 54,840 | 14,370 | 7,720 |
| 1500 | 33,870 | 32,820 | 65,770 | 56,970 | 61,570 | 52,770 | 70,180 | 61,380 | 65,980 | 57,180 | 15,400 | 7,920 |
| 1600 | 35,490 | 34,370 | 68,540 | 59,500 | 64,060 | 55,020 | 73,050 | 64,020 | 68,570 | 59,540 | 16,420 | 8,110 |
| 1700 | 37,250 | 36,060 | 71,710 | 62,370 | 66,950 | 57,610 | 76,390 | 67,050 | 71,630 | 62,290 | 17,440 | 8,400 |
| 1800 | 39,060 | 37,800 | 74,950 | 65,270 | 69,910 | 60,230 | 79,780 | 70,110 | 74,740 | 65,070 | 18,480 | 8,690 |
| 1900 | 40,460 | 39,130 | 77,190 | 67,410 | 71,870 | 62,090 | 82,080 | 72,300 | 76,760 | 66,990 | 19,500 | 9,270 |
| 2000 | 42,270 | 40,870 | 80,420 | 70,310 | 74,820 | 64,710 | 85,470 | 75,360 | 79,870 | 69,760 | 20,600 | 9,560 |

NOTE: The BTU figures in this table are based upon AHRI NET calculations where ceiling height is 8 ft. and where total window and door areas do not exceed 20 percent of the GROSS wall area. For 9 ft. ceiling height add 11 percent to heat loss; for 10 ft. ceiling height, add 22 percent. For lower levels ONE HALF or LESS below grade level, use FIRST FLOOR heat loss.

TABLE C: DESIGN TEMPERATURE CORRECTION FACTORS (For other than 70° Design Temperature Difference)

| DESIGN TEMP. DIFFERENCE | FACTOR | DESIGN TEMP. DIFFERENCE | FACTOR | DESIGN TEMP. DIFFERENCE | FACTOR |
|----------------------------|--------|----------------------------|--------|----------------------------|--------|
| 25°F | .35 | 55°F | .78 | 90°F | 1.29 |
| 30°F | .42 | 60°F | .85 | 95°F | 1.36 |
| 35°F | .50 | 65°F | .92 | 100°F | 1.43 |
| 40°F | .57 | 75°F | 1.07 | 105°F | 1.50 |
| 45°F | .64 | 80°F | 1.15 | 110°F | 1.57 |
| 50°F | .71 | 85°F | 1.20 | 115°F | 1.64 |

Note: Conversion factor for "in between" temperatures can be determined by interpolation between the closest tabulated values. Example: the outdoor design temperature in Philadelphia, PA is 14°F. Indoor minus outdoor temperature equals 56°F. Interpolated factor equals 0.79 (rounded).

TABLE D: CEILING CORRECTION FACTORS (For first floor heat loss in two story structure)

| CONSTRUCTION DESIGN NO. | FACTOR |
|----------------------------|--------|----------------------------|--------|----------------------------|--------|----------------------------|--------|
| 1 | .82 | 7 | .88 | 13 | .94 | 19 | .82 |
| 2 | .79 | 8 | .86 | 14 | .83 | 20 | .89 |
| 3 | .88 | 9 | .91 | 15 | .80 | 21 | .88 |
| 4 | .86 | 10 | .94 | 16 | .88 | 22 | - |
| 5 | .83 | 11 | .86 | 17 | .87 | 23 | - |
| 6 | .82 | 12 | .91 | 18 | .84 | | |

STEP 3: SELECT THE BOILER

The size of the replacement boiler will be based on the Total Heat Loss of the building calculated in Step 2. The boiler should be selected based on its AHRI NET Rating in BTU/Hr. For example, if the Total Heat Loss of the house is 85,000 BTU/ Hr. then the AHRI NET Rating of the replacement boiler must be at least 85,000. It can be morebut **never** less.

For convenience, Table E (opposite page) shows the Net AHRI NET water ratings for current Weil-McLain gas and oil boilers for homes and small commercial buildings.

STEP 4: DETERMINE THE BID PRICE

Figure 3 (opposite page) is a general checklist of the materials which may be required for a boiler replacement job (also part of the Weil-McLain Boiler Replacement Worksheet). This list can be used to figure the cost of all materials as well as labor, overhead, and profit.

TABLE E: AHRI NET RATINGS IN BTU/HR. FOR WEIL-McLAIN BOILERS NOTE: Always consult product manual for details

| Evergreen® | | | | | | |
|------------|--------------|-------|--|--|--|--|
| MODEL | WATER RATING | AFUE | | | | |
| EVG 110 | 88,000 | 95.0 | | | | |
| EVG 155 | 124,000 | 95.1 | | | | |
| EVG 220 | 179,000 | 95.0 | | | | |
| EVG 299 | 243,000 | 95.0 | | | | |
| EVG 399 | 333,000 | 96.5* | | | | |

| Ultra™ | | |
|---------|--------------|--------|
| MODEL | WATER RATING | AFUE |
| ULT 80 | 62,000 | 93.5% |
| ULT 105 | 81,000 | 94.0% |
| ULT 155 | 123,000 | 94.0% |
| ULT 230 | 183,000 | 94.1% |
| ULT 299 | 234,000 | 92.5% |
| ULT 399 | 317,000 | 91.7%* |

| GV90+* | | | | | | |
|--------|--------------|-------|--|--|--|--|
| MODEL | WATER RATING | AFUE | | | | |
| GV90+3 | 56,000 | 91.9% | | | | |
| GV90+4 | 84,000 | 91.2% | | | | |
| GC90+5 | 113,000 | 91.4% | | | | |
| GV90+6 | 140,000 | 91.0% | | | | |

| CGi | | |
|--------|--------------|------|
| MODEL | WATER RATING | AFUE |
| CGi-25 | 35,000 | 84% |
| CGi-3 | 42,000 | 84% |
| CGi-4 | 66,000 | 84% |
| CGi-5 | 88,000 | 84% |
| CGi-6 | 117,000 | 84% |
| CGi-7 | 140,000 | 84% |
| CGi-8 | 164,000 | 84% |

| ECO [®] Tec | | | | | | | |
|----------------------|--------------|------|--|--|--|--|--|
| MODEL | WATER RATING | AFUE | | | | | |
| ET 80-H | 64,000 | 95% | | | | | |
| ET 110-H | 87,000 | 95% | | | | | |
| ET 150-H | 121,000 | 95% | | | | | |
| ET 199-H | 160,000 | 95% | | | | | |
| ET 110-C | 87,000 | 95% | | | | | |
| ET 150-C | 121,000 | 95% | | | | | |
| ET 199-C | 160,000 | 95% | | | | | |

| AquaBalance [®] | | | | | | |
|--------------------------|-----------------|------|--|--|--|--|
| MODEL | WATER RATING | AFUE | | | | |
| AB-80H | 65,000 | 95% | | | | |
| AB-120H | 97,000 | 95% | | | | |
| AB-155H | 125,000 | 95% | | | | |
| AB-80C | 65,000 | 95% | | | | |
| AB-120C | 97,000 | 95% | | | | |
| AB-155C | 125,000 | 95% | | | | |

| CGa | | |
|--------|--------------|------|
| MODEL | WATER RATING | AFUE |
| CGa-25 | 27,000 | 84% |
| CGa-3 | 48,000 | 84% |
| CGa-4 | 73,000 | 84% |
| CGa-5 | 98,000 | 84% |
| CGa-6 | 122,000 | 84% |
| CGa-7 | 147,000 | 84% |
| CGa-8 | 172,000 | 84% |

| EG - Water | | | | | | | |
|------------|--------------|-------|--|--|--|--|--|
| MODEL | WATER RATING | AFUE | | | | | |
| EG-30 | 55,000 | 84.3% | | | | | |
| EG-35 | 73,000 | 83.6% | | | | | |
| EG-40 | 91,000 | 84.0% | | | | | |
| EG-45 | 110,000 | 83.5% | | | | | |
| EG-50 | 128,000 | 83.8% | | | | | |
| EG-55 | 146,000 | 83.8% | | | | | |
| EG-65 | 183,000 | 84.0% | | | | | |
| EG-75 | 217,000 | 82.7% | | | | | |

| 80 | |
|-------|--------------|
| MODEL | WATER RATING |
| 380 | 242,000 |
| 480 | 344,000 |
| 580 | 448,000 |
| 680 | 551,000 |
| 780 | 655,000 |
| 880 | 758,000 |
| 980 | 862,000 |
| 1080 | 965,000 |
| 1180 | 1,069,000 |
| 1280 | 1,172,000 |

| SVF™ | | |
|----------|--------------|---------|
| MODEL | WATER RATING | AFUE |
| SVF 750 | 657,000 | 96.3%* |
| SVF 1000 | 842,000 | 96.8%* |
| SVF 1100 | 957,000 | 97.1%* |
| SVF 1500 | 1,259,000 | 96.5%* |
| SVF 2000 | 1,672,000 | 96.2%* |
| SVF 2500 | 2,104,000 | 96.8%* |
| SVF 3000 | 2,499,000 | 95.8%** |

| SLIM FIT® | | |
|-----------|--------------|--------|
| MODEL | WATER RATING | AFUE |
| SF-550 | 450,000 | 93.9%* |
| SF-750 | 610,000 | 93.6%* |
| SF-1000 | 833,000 | 95.8%* |
| SF-1500 | 1,250,000 | 95.9%* |
| SF-2000 | 1,657,000 | 95.8%* |

* Indicates Thermal Efficiency Rating ** Indicates Combustion Efficiency Rating

FIGURE 3: MATERIAL LIST

| QTY | ITEM | AMOUNT | QTY | AFUE | AMOUNT |
|-----|---------------------------------------|--------|-----|------------------------|--------|
| | Boiler No. | | | Copper Pipe: ½" | |
| | Thermostats | | | 3⁄4″ | |
| | Zone Valves | | | 1″ | |
| | Balancing Valves | | | 11⁄4″ | |
| | Expansion Tank | | | 11⁄2″ | |
| | Flow Control Valve | | | Fittings | |
| | Low Limit or Reverse Acting Control | | | | |
| | Pressure Reducing Valve | | | | |
| | Flue Pipe | | | | |
| | Extra Valves | | | | |
| | Gas Piping | | | Electric Wiring | |
| | Oil Tank, Pipe and Fittings | | | Freight and Cartage | |
| | Insulated Domestic Water Storage Tank | | | | |
| | Domestic Water Coil | | | | |
| | Pipe | | | Incidentals | |
| | Fuel Valves | | | | |
| | Circulators | | | TOTAL COST OF MATERIAL | |
| | Relay | | | Labor | |
| | Circuit Braker (or fuse) Panel | | | Profit | |
| | 240v. Disconnect Switch | | | Overhead | |
| | 240v. 3-Wire Service Cable | | | | |
| | SUB-TOTAL | | | BID PRICE | |

SAMPLE PROBLEM

STEP 1: COMPLETE A JOB SURVEY FORM

A properly completed Job Survey Form is shown in Figure 4. The Key Information:

- Two story house with unheated basement-816 sq. ft. of floor space each level.
- Construction: 4" brick and 4" light weight block, furred, lath and plaster; 3" ceiling insulation; double glass, weatherstripped.
- 80°F design temperature difference.
- Type of System: series loop.
- Type of Radiation: convector baseboard.
- Owner wants to replace his old boiler with a new high efficiency gas fired water boiler. Owner wants night set-back thermostat.

FIGURE 4: JOB SURVEY FORM

| BOILER REPLACEMENT WORKSHEET |
|---|
| JOB SURVEY FORM CUSTOMER NAME: <u>C. L. Jones</u> PHONE: <u>327-9489</u> |
| ADDRESS: 18075 Ski Run Drive, Monroe |
| PREPARED BY: RKT DATE: 2/15 |
| PRESENT HEATING SYSTEM: Series loop |
| TYPE OF RADIATION: Convector BSBD |
| HEATING MEDIUM: 🛛 🖾 Hot Water 🗆 Steam |
| FUEL NOW USED: 🛛 🖄 Natural Gas 🗆 Propane 🗆 #2 Oil 🛛 🗆 Electricity |
| FUEL TO BE USED: 🛛 Natural Gas 🗆 Propane 🗆 #2 Oil 🔅 Electricity |
| IS SYSTEM HEATING SATISFACTORILY? |
| If no, what is the problem? |
| How can it be corrected? |
| RELOCATE BOILER? Yes Kan No If yes estimate time Materials |
| Corrosive Atmosphere? no |
| PRESENT SOURCE OF DOMESTIC WATER: Tankless Heater Indirect Tank Other Separate |
| WILL NEW BOILER HAVE A WATER HEATER? 🛛 Yes 🛛 No 🛛 Type |
| HOUSE CONSTRUCTION: |
| GLASS: <u>double glass, weatherstripped</u> |
| WALLS: <u>4" brick, 4" block — furred, lath & plaster</u> |
| CEILING: <u>3" insulation</u> |
| SLAB: wood over bsmt. |
| HOUSE DIMENSIONS (Use sketch for accuracy): |
| High Altitude Ft. Elevation |
| Basement <u>8</u> ' H x <u>34</u> ' L x <u>24</u> ' W = <u>816</u> Sq. Ft. |
| First Floor <u>8</u> ' H x <u>34</u> ' L x <u>24</u> ' W = <u>816</u> Sq. Ft. Second Floor <u>8</u> ' H x <u>34</u> ' L x <u>24</u> ' W = <u>816</u> Sq. Ft. |
| Second Floor <u>6</u> H x <u>54</u> L x <u>24</u> W = <u>616</u> Sq. Ft. DESIGN TEMPERATURE DIFFERENCE <u>80</u> °F |
| NEW THERMOSTAT(S) REQUIRED |
| |

STEP 2: CALCULATE TOTAL HEAT LOSS

The Total Heat Loss for the example is calculated on the form shown in Figure 5 based on the following steps:

- 1. The construction of the house matches Construction Design Number 17 in Table A (page 4).
- 2. Each of the two levels is rounded to 800 sq ft (the basement is not heated).
- 3. From Table B (page 5) Construction No. 17 at 800 sq ft has a heat loss of 33,430 BTU/Hr.
- Table C (page 6) shows a 1.15 correction factor for 80°F Design Temperature Difference. Therefore, the heat loss for each area is 38,450 BTU/Hr. (33,430 x 1.15 rounded).
- 5. Since it is a two story house, the first floor does not have a ceiling loss. Table D (page 6) indicates a Ceiling

Correction Factor for Construction Number 17 of .87. Therefore, the total adjusted heat loss for the first floor is 33,450 BTU/Hr. (38,450 x .87 rounded).

6. The total heat loss for the two levels is 71,900 BTU/Hr.

STEP 3: SELECT THE BOILER

The Total Heat Loss of 71,900 BTU/Hr. calculated in Step 2 is the minimum AHRI NET Rating of the new boiler. The owner wants a high efficiency gas boiler. Therefore, from Table E (page 7) the Ultra 105, WM97+ 110, ECO 110, GV90+ 4, CGi-5, CGa-4, or EG 40 could be selected. The Model Number of the boiler would be recorded on the Materials List. (Figure 3, page 7). The list would then be used to calculate material cost; add labor, overhead and profit; and determine the selling price.

| LEVEL | CONSTRUCTION NUMBER | SQ. FT. | HEAT LOSS (AT 70°F DESIGN TEMP. DIFF.) | CORREC FACTOR 80 | | ΤΟΤΑΙ | _ | CEILING CORRECTION FACTOR | ADJUSTED HEAT LOSS |
|--------------|------------------------|---------|---|------------------------|-----|--------|------|---------------------------------|-----------------------|
| FIRST LEVEL | 17 | 800 | _33,430 x | 1.15 | _ = | 38,450 | x | .87 = | 33,450 |
| SECOND LEVEL | 17 | 800 | <u>33,430</u> x | 1.15 | _ = | 38,450 | | | 38,450 |
| MID-LEVEL | | | X | | = | | | | |
| BASEMENT | | | x | | = | | | | |
| SLAB | | | x | | = | | | | |
| | | | | | | | тоти | AL HEAT LOSS | 71,900 |

SECTION 2 PROCEDURE FOR SIZING STEAM BOILERS

To properly size a replacement steam boiler, determine the total BTU capacity of the connected radiation in the building. This method is necessary so that the new boiler will

produce adequate steam to fill the entire system. To make the calculations, determine the number of square feet of direct radiation in **each** radiator connected to the existing boiler. Follow these steps:

1. Identify the style of the radiator. Figure 6 shows the



relative sizes of three different radiator styles. All are four tube, eight section radiators but the rating of each is different.

- 2. Measure the height and width of the radiator.
- 3. Count the number of tubes in each section.
- 4. Count the number of sections.
- 5. Determine the square feet of radiation in each section. See Table F (page 10).
- 6. Multiply the square feet of radiation in each section by the number of sections.
- 7. Total the square feet of radiation for all the radiators in the building.

FIGURE 5: HEAT LOSS CALCULATION FORM

- 8. Convert the total square feet of radiation to BTU/Hr. Each square foot of steam radiation is based on a heat emission of 240 BTU/Hr. with standard 70°F air temperature and 215°F steam temperature in the radiator.
- 9. Size the replacement steam boiler by selecting a unit with a AHRI NET Steam rating equal to or greater than the BTU/Hr. capacity of the radiation.

EXAMPLE:

Figure 7 is a tube type radiator, 20" high by 7" wide. There are 4 tubes per section and 8 sections. Table F shows this size tube type radiator has 2 1/4 square feet of radiation per section. 2 ¼ times





8 (the number of sections) equals 18 square feet of direct radiation. 18 times 240 (BTU/Hr.) equals 4,320 BTU/Hr. for this radiator.

TABLE F: SQUARE FEET OF RADIATION PER RADIATOR SECTION

| | OLD STYLE COLUMN RADIATORS | | | | | | | | | |
|-------------------------|----------------------------|-------------|------|-------------|-------------|-------------|--|--|--|--|
| NO. OF TUBES OR COLUMNS | | | | | | | | | | |
| | 1 | 1 2 3 4 5 6 | | | | | | | | |
| WIDTH (IN.) | 4 ½ | 7 ¾ | 9 | 11 ½ | 12 ½ | 12 ½ | | | | |
| HEIGHT (IN.) | | | | | | | | | | |
| 45 | 31⁄2 | 5 | 6 | 10 | - | - | | | | |
| 38 | 3 | 4 | 5 | 8 | 10 | - | | | | |
| 32 | 21⁄2 | 31⁄3 | 41⁄2 | 6½ | 81⁄2 | - | | | | |
| 26 | 2 | 2²/3 | 3¾ | 5 | 7 | 7 | | | | |
| 23 | 12/3 | 21/3 | 3¼ | 41⁄2 | - | - | | | | |
| 22 | 12/3 | 21⁄4 | 3 | 4 | 6 | 6 | | | | |
| 20 | 11⁄2 | 2 | 23⁄4 | 31/2 | 5 | 5 | | | | |
| 18 | 11⁄3 | 13⁄4 | 21⁄4 | 3 | 5 | 41⁄3 | | | | |
| 17 | - | - | - | - | - | 4 | | | | |
| 16 | - | - | - | - | 4 | 3¾ | | | | |
| 15 | - | 11/2 | - | - | - | - | | | | |
| 14 | - | - | - | - | 4 | 3 | | | | |
| 13 | - | - | - | - | 3 | 3 | | | | |

| TUBE TYPE RADIATORS | | | | | | | | | | |
|---------------------|------------|-----------|--------------------------|--------------------------|--------------------------------------|--|--|--|--|--|
| NO. OF TUBES | | | | | | | | | | |
| | 3 | 3 4 5 6 7 | | | | | | | | |
| WIDTH (IN.) | 5 | 7 | 8 ³ ⁄4 | 9 ³ ⁄4 | 12 ½ | | | | | |
| HEIGHT (IN.) | | | | | | | | | | |
| 38 | 3½ | 4¼ | 5 | 6 | - | | | | | |
| 36 | 31⁄2 | 4¼ | 5 | 6 | 7 | | | | | |
| 32 | 3 | 3½ | 41⁄3 | 5 | 6 | | | | | |
| 26 | 2 ½ | 23⁄4 | 3½ | 4 | 5 | | | | | |
| 23 | 2 | 21⁄2 | 3 | 3½ | 41⁄2 | | | | | |
| 22 | - | - | - | - | 41⁄2 | | | | | |
| 20 | 13⁄4 | 21⁄4 | 2 ² /3 | 3 | 3 ² / ₃ | | | | | |
| 18 | - | - | - | - | 31/2 | | | | | |
| 17 | - | - | - | - | 3 | | | | | |
| 16 | - | - | - | - | 3 | | | | | |
| 14 | - | - | - | - | 21/2 | | | | | |

| | тні | N TUBE R | ADIATOR | S | |
|-----------------|------------|----------|--------------------------|---|------|
| | | NO. OF | TUBES | | |
| | 2 | 3 | 4 | 5 | 6 |
| WIDTH (IN.) | 3 ½ | 4 | 4 ³ ⁄4 | 6 | 7% |
| HEIGHT (IN.) | | | | | |
| 38 | 21⁄2 | 2²/3 | - | - | - |
| 32 | 2 | 21⁄3 | - | - | 32/3 |
| 26 | - | - | 2 ⅓ | 3 | 3 |
| 25 | 11/2 | 12/3 | 2 | - | 3 |
| 23 | - | - | - | 2 | - |
| 22 | 11⁄3 | 11/3 | 14⁄5 | - | - |
| 20 | - | - | 14⁄5 | - | 21⁄3 |
| 19 | 1 | 11⁄4 | 12/3 | - | 21⁄3 |
| 17 | - | - | - | 2 | - |

| WALL TYPE RADIATORS | |
|---------------------|-------------------------|
| SIZE | SQ. FT. PER RADIATOR |
| 13½" x 17" x 3" | 5 |
| 13½" x 21" x 3" | 6 |
| 13½" x 22" x 3" | 7 |
| 13½" x 29" x 3" | 9 |



| SECTIONAL WALL TYPE RADIATORS | | |
|----------------------------------|-------------------------------------|--|
| HEIGHT (IN.) | SQ. FT. RADIATION PER SECTION | |
| 37 | 21⁄2 | |
| 26½ | 14⁄s | |
| 21½ | 11⁄2 | |
| 15 | 1 | |
| 137⁄8 | 3⁄4 | |

| CAST IRON BASEBOARD | |
|---------------------|----------------------|
| HEIGHT (IN.) | SQ. FT. RADIATION |
| 7 | 2.40 |
| 9 | 3.35 |

APPENDIX OTHER CONSIDERATIONS IN BOILER REPLACEMENT

1. INSTALLATION INSTRUCTIONS

In order for the warranty on a new boiler to be honored, the boiler must be installed in strict accordance with the manufacturer's installation instructions. It is imperative that the heating contractor follows the instructions furnished with the equipment. If questions arise, the heating contractor should contact the distributor.

2. GRAVITY SYSTEMS

Adding a circulator to a gravity system may improve circulation in areas that had poor circulation; however the circulator will not increase the amount of heat available per unit of time. The circulator should be operated with a reverse acting control to turn it ON when system water temperature reaches 110-120°F; OFF at about 90-100°F.

3. STEAM HEATING SYSTEMS

Be sure to check the following:

- (a) total square feet of installed radiation,
- (b) modifications to the system from its original condition,
- (c) physical condition of the system,
- (d) condensate return time (slow?),
- (e) if the low water cutoff is activated frequently (f) if there is a pump control to operate the condensate pump.

(g) the possibility of buried (leaking) piping. Also, check the boiler water for contaminants by boiling two water samples in separate pans-one sample of tap water and one of boiler water. If the boiler water foams over like boiled milk, the water is contaminated and should be treated accordingly.

4. CLEANING STEAM BOILERS

The proper cleaning of new steam boilers is perhaps the most neglected step in steam boiler replacement. It is also a factor many installers overlook when estimating the cost of the job. After installation, a steam boiler should be cleaned and flushed. Chemical additives for cleaning or water treatment must be carefully considered. When in doubt, consult a reputable water treatment firm, or Weil-McLain since most chemicals generally cause more problems than they solve and can void the warranty. Never use petroleum products. In addition, a thorough check of the valves, vents and traps should be made to be sure they are in good working order and are the type and size needed for the application.

5. CLEANING HOT WATER SYSTEMS

Old hot water systems may have mud, sludge or other accumulation which could affect the operation of a new boiler. If there is any evidence of deposits in the old boiler when it is removed, the piping and radiation should be flushed with cold water before the material hardens.

6. EXPANSION TANKS

New water boilers must be installed with a properly sized expansion tank in order to avoid the loss of system water during each warm-up cycle and the replacement of the lost water with fresh makeup water with the pressure reducing valve. The frequent addition of makeup water to a heating system can cause severe damage and must be prevented.

7. THERMOSTATS

Modern controls on a new boiler will usually require a different heat anticipator setting for the thermostat. Many older thermostats either have fixed-heat anticipators-or none at all. For proper boiler operation and owner satisfaction, the thermostat heat anticipator must be set properly. Follow instructions.

OUTDOOR DESIGN TEMPERATURES FOR SELECTED CITIES

| ALABAMA | |
|---|---|
| Anniston | .22 |
| Birmingham | . 21 |
| Mobile | |
| Montgomery | |
| ALASKA | |
| Anchorage | -18 |
| Fairbanks | |
| Juneau. | |
| Nome | |
| ARIZONA | 27 |
| Flagstaff | 4 |
| Phoenix | |
| Tucson | |
| Winslow | |
| Yuma | |
| ARKANSAS | .55 |
| Fort Smith | 17 |
| Little Rock | |
| | .20 |
| Bakersfield | 70 |
| Eureka | |
| | |
| Fresno | |
| Los Angeles | |
| Oakland | |
| Sacramento | |
| San Diego | |
| San Francisco | |
| San Jose | .36 |
| COLORADO | |
| Denver | |
| Grand Junction | |
| Pueblo | 0 |
| CONNECTICUT | |
| | |
| Hartford | |
| New Haven | |
| New Haven | 7 |
| New Haven DELAWARE Dover | 7 . 15 |
| New Haven DELAWARE Dover | 7 . 15 |
| New Haven DELAWARE Dover Wilmington DISTRICT OF COLUMBIA | 7 . 15 . 14 |
| New Haven DELAWARE Dover Wilmington DISTRICT OF COLUMBIA Washington | 7 . 15 . 14 |
| New Haven DELAWARE Dover Wilmington DISTRICT OF COLUMBIA Washington FLORIDA | 7 . 15 . 14 . 14 |
| New Haven DELAWARE Dover Wilmington DISTRICT OF COLUMBIA Washington FLORIDA Jacksonville | 7 . 15 . 14 . 14 . 32 |
| New Haven DELAWARE Dover Wilmington DISTRICT OF COLUMBIA Washington FLORIDA Jacksonville Miami | 7 . 15 . 14 . 14 32 47 |
| New Haven DELAWARE Dover | 7 . 15 . 14 . 14 32 47 29 |
| New Haven DELAWARE Dover | 7 . 15 . 14 . 14 32 47 29 |
| New Haven | 7 . 15 14 14 32 47 29 .40 |
| New Haven DELAWARE Dover | 7 . 15 14 14 32 47 29 .40 |
| New Haven | 7 15 14 14 32 47 29 40 22 |
| New Haven DELAWARE Dover | 7 15 14 14 32 47 29 40 22 23 |
| New Haven DELAWARE Dover | 7 15 14 14 32 47 29 40 22 23 25 |
| New Haven DELAWARE Dover Wilmington DISTRICT OF COLUMBIA Washington FLORIDA Jacksonville Miami Pensacola Tampa GEORGIA Atlanta Augusta Macon | 7 15 14 14 32 47 29 40 22 23 25 |
| New Haven DELAWARE Dover Wilmington DISTRICT OF COLUMBIA Washington FLORIDA Jacksonville Miami Pensacola Tampa GEORGIA Atlanta Augusta Macon Savannah IDAHO | 7 15 14 14 32 47 29 40 22 23 25 27 |
| New Haven DELAWARE Dover | 7 15 14 14 32 47 29 40 22 23 25 27 10 |
| New Haven | 7 15 14 14 32 47 29 40 22 23 25 27 10 1 |
| New Haven | 7 15 14 14 29 40 22 27 10 1 6 |
| New Haven DELAWARE Dover Wilmington DISTRICT OF COLUMBIA Washington FLORIDA Jacksonville Miami Pensacola Tampa . GEORGIA Atlanta. Augusta. Macon Savannah IDAHO Boise Coeur D'Alene Lewiston | 7 15 14 14 29 40 22 27 10 1 6 |
| New Haven | 7 15 14 14 32 47 29 40 22 27 10 1 6 1 |
| New Haven | 7 15 14 14 29 40 22 23 27 0 10 1 |
| New Haven | 7 .15 .14 .14 .32 .47 .29 40 .22 .23 .25 .27 .10 1 0 4 |
| New Haven | 7 .15 .14 14 29 27 29 27 10 1 6 1 0 4 4 |
| New Haven | 7 15 14 14 29 23 25 27 0 1 0 4 4 2 |
| New Haven | 7 15 14 14 29 23 25 27 0 1 0 4 4 2 |
| New Haven | 7 15 14 14 29 40 22 23 25 27 10 1 0 4 2 2 |
| New Haven | 7 15 14 14 29 40 22 27 0 4 1 |
| New Haven | 7 15 14 14 29 40 22 27 0 4 1 |
| New Haven | 7 15 14 14 29 27 29 27 27 27 1 2 2 2 |
| New Haven | 7 15 14 14 29 23 25 27 0 1 0 1 0 1 0 4 2 |
| New Haven | 7 15 14 14 29 23 25 27 0 1 0 1 0 1 0 1 0 1 2 2 2 2 2 2 |
| New Haven | 7 .15 .14 .14 .32 .47 .29 40 .22 .23 .25 .27 .10 1 0 4 1 0 4 2 2 2 2 2 2 |

| KANSAS | |
|--|--|
| | |
| Dodge City | 5 |
| 0, | |
| Topeka | |
| Wichita | .7 |
| KENTUCKY | |
| Louisville | 10 |
| | 10 |
| LOUISIANA | |
| New Orleans | 33 |
| Shreveport | |
| | 20 |
| MAINE | |
| Augusta | -3 |
| Bangor | -6 |
| 5 | -13 |
| | |
| Portland | 1 |
| MARYLAND | |
| | 17 |
| Baltimore | 15 |
| MASSACHUSETTS | |
| Boston | .9 |
| Nantucket | |
| | |
| Springfield | .0 |
| Worcester | .4 |
| MICHIGAN | |
| | _ |
| Battle Creek | |
| Detroit | .6 |
| Flint | 1 |
| | |
| Grand Rapids | |
| Lansing | . 1 |
| Sault St. Marie | -8 |
| MINNESOTA | - |
| | |
| Duluth | 16 |
| Minneapolis | -12 |
| Hibbing: | |
| | 20 |
| MISSISSIPPI | |
| Meridian | 23 |
| Vicksburg | 26 |
| MISSOURI | |
| | |
| Columbia | .4 |
| | |
| Kansas Citv | |
| Kansas City | .6 |
| St. Louis | .6 |
| - | .6 |
| St. Louis | .6 .6 |
| St. Louis | .6 .6 10 |
| St. Louis MONTANA Billings Butte | .6 .6 10 .17 |
| St. Louis | .6 .6 10 .17 .16 |
| St. Louis | .6 .6 10 .17 .16 .7 |
| St. Louis | .6 .6 10 .17 .16 .7 |
| St. Louis MONTANA Billings. Butte Helena Kalispell. Miles City | .6 .6 10 .17 .16 .7 |
| St. Louis | .6 .6 10 .17 16 -7 .15 |
| St. Louis | .6 .6 10 -17 16 -7 -15 |
| St. Louis | .6 .6 10 -17 16 -7 -15 |
| St. Louis | .6 .6 10 .17 .16 .7 .15 .2 .2 |
| St. Louis | .6 .6 10 .17 .16 .7 .15 .2 .2 |
| St. Louis | .6 .6 10 -17 -16 -7 -15 -2 -4 -3 |
| St. Louis | .6 .6 10 -17 -16 -7 -15 -2 -4 -3 |
| St. Louis | .6 .6 10 -17 16 -7 -15 -2 -4 -3 28 |
| St. Louis | .6 .6 10 .17 .16 -7 .15 -2 -4 -3 28 |
| St. Louis | .6 .6 10 .17 .16 -7 .15 -2 -4 -3 28 |
| St. Louis | .6 .6 10 -17 16 -7 -15 -2 -4 -3 28 10 .3 |
| St. Louis | .6 .6 10 .17 .16 -7 .15 -2 -4 -3 28 0 .3 -3 |
| St. Louis | .6 .6 10 .17 .16 -7 .15 -2 -4 -3 28 0 .3 -3 |
| St. Louis | .6 .6 10 .17 .16 -7 .15 -2 -4 -3 28 0 .3 -3 |
| St. Louis | .6 .6 10 .17 .16 .7 .15 .2 .4 .3 .3 .3 .3 |
| St. Louis | .6 .6 10 .17 .16 .7 .15 .2 .4 .3 .3 .3 .3 .3 .13 |
| St. Louis | .6. .6. 10.17.16.7.15 -2.4.3.28.10.3 -3.3.13.14 |
| St. Louis | .6. .6. 10.17.16.7.15 -2.4.3.28.10.3 -3.3.13.14 |
| St. Louis | .6. .6. 10.17.16.7.15 -2.4.3.28.10.3 -3.3.13.14 |
| St. Louis | .6 .6 10 -17 16 -7 -15 -2 -4 -3 28 0 .3 -3 13 14 14 |
| St. Louis | .6 .6 .10 .17 .16 .7 .15 .2 .4 .3 .3 .3 .13 .14 .14 .16 |
| St. Louis | .6 .6 .10 .17 .16 .7 .15 .2 .4 .3 .3 .3 .13 .14 .14 .16 |
| St. Louis | .6 .6 .10 .17 .16 .7 .15 .2 .4 .3 .3 .3 .13 .14 .14 .16 |
| St. Louis | .6. .6. 10-17-16-7-15-2-4-3-28-10.3-3-3-13-14-14-16-18 |
| St. Louis | .6. .6. 10.77. 10.77. 10.7 |
| St. Louis | .6. .6. 10.77. 10.77. 10.7 |
| St. Louis | .6. .6. 10.77. 16.7. .7. .2. .2. 28. 10.3. .3. .3. .1. 14.4. 16.8. .1. |
| St. Louis | .6. .6. 10716-7-15 -2-4-3 2810.3 -3-3 131414 16181. .6. |
| St. Louis | .6. 10716-7-15 -2-4-3 2210.3 -3-3 131414 1618 -1.1.6.8 |
| St. Louis | .6. 0171675 -243 28103 -33 131414 1618 -1.1.6-815 |
| St. Louis | .6. 0171675 -243 28103 -33 131414 1618 -1.1.6-815 |
| St. Louis | .6.6 101716775 2243 28103 33 131414 1618 .1.1.6.8155 |

| NORTH CAROLINA | |
|--|---|
| Asheville | . 14 |
| Charlotte | .22 |
| Greensboro | . 18 |
| Raleigh | |
| Wilmington | .26 |
| NORTH DAKOTA | |
| Bismarck | |
| Fargo | -18 |
| OHIO Akron | e |
| Cincinnati | |
| Cleveland | |
| Columbus | |
| Dayton | |
| Sandusky | |
| Toledo | 1 |
| OKLAHOMA | |
| Oklahoma City | . 13 |
| Tulsa | |
| OREGON | |
| Baker | |
| Eugene | |
| Medford | |
| Portland | |
| Salem | .23 |
| PENNSYLVANIA | ~ |
| Erie | |
| Harrisburg | |
| Philadelphia | |
| Scranton | |
| RHODE ISLAND | 5 |
| Providence | q |
| SOUTH CAROLINA | |
| Charleston | |
| | .27 |
| | |
| Columbia | .24 |
| | .24 |
| Columbia | .24 .22 |
| Columbia Greenville SOUTH DAKOTA Huron Pierre | .24 .22 -14 -10 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. | .24 .22 -14 -10 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE | .24 .22 -14 -10 7 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre Rapid City. TENNESSEE Chattanooga | .24 .22 -14 -10 7 .18 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. | .24 .22 -14 -10 7 . 18 . 19 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. | .24 .22 -14 -10 7 . 18 . 19 . 18 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville | .24 .22 -14 -10 7 . 18 . 19 . 18 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville Memphis Nashville. TEXAS | .24 .22 -14 -10 7 . 18 . 19 . 18 . 14 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville. TEXAS Abilene | .24 .22 -14 -10 7 . 18 . 19 . 18 . 14 .20 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre Rapid City. TENNESSEE Chattanooga Knoxville Memphis Nashville TEXAS Abilene Amarillo. | .24 .22 -14 -10 7 . 18 . 19 . 18 . 14 .20 11 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre Rapid City. TENNESSEE Chattanooga Knoxville Memphis Nashville TEXAS Abilene Amarillo. Austin | .24 .22 -14 -10 7 . 18 . 19 . 18 . 14 .20 11 .33 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville. Nashville. Abilene Amarillo. Austin Brownsville. | .24 .22 -14 -10 .77 .18 .19 .18 .14 .20 11 .33 .39 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville Memphis. Nashville. TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi | .24 .22 -14 -10 .7 .18 .19 .18 .14 .20 11 .33 .39 .35 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville. TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi Dallas. | .24 .22 -14 -10 .7 .18 .19 .18 .14 .20 .33 .39 .35 .22 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville Memphis. Nashville. TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi | .24 .22 -14 -10 .77 .18 .19 .18 .14 .20 11 .33 .39 .35 .22 .31 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville. TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi Dallas. Del Rio. | .24 .22 -14 -10 .77 .18 .19 .18 .14 .20 11 .33 .39 .35 .22 .31 .24 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre Rapid City. TENNESSEE Chattanooga Knoxville Memphis Nashville TEXAS Abilene Amarillo. Austin Brownsville Corpus Christi Dallas. Del Rio. El Paso. | .24 .22 -14 -10 .7 .18 .19 .18 .14 .20 11 .33 .39 .35 .22 .31 .24 .22 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre Rapid City. TENNESSEE Chattanooga Knoxville Memphis. Nashville TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. | .24 .22 -14 -10 .7 .18 .19 .18 .14 .20 .11 .33 .39 .35 .32 .31 .24 .22 .36 .32 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre Rapid City. TENNESSEE Chattanooga Knoxville Memphis. Nashville TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. Galveston | .24 .22 -14 -10 .7 .18 .19 .18 .14 .20 .11 .33 .39 .22 .31 .24 .22 .36 .32 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville. TEXAS Abilene. Austin. Brownsville. Corpus Christi. Dallas. Del Rio. El Paso. Ft. Worth. Galveston. Houston. Port Arthur. San Antonio. | .24 .22 -14 -10 .7 .18 .19 .18 .14 .20 .11 .33 .22 .31 .22 .36 .32 .31 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre Rapid City. TENNESSEE Chattanooga Knoxville Memphis Nashville TEXAS Abilene Amarillo. Austin Brownsville Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. Galveston Houston. Port Arthur San Antonio. UTAH | .24 .22 -14 -10 .7 .18 .19 .18 .14 .20 11 .33 .39 .35 .22 .31 .24 .22 .36 .32 .30 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre Rapid City. TENNESSEE Chattanooga Knoxville Memphis Nashville TEXAS Abilene Amarillo. Austin Brownsville Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. Galveston Houston. Port Arthur San Antonio. UTAH Salt Lake City. | .24 .22 -14 -10 . 7 . 18 . 19 . 18 . 14 . 20 11 .33 .35 .22 . 31 .24 .22 .36 .32 .32 .30 8 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre Rapid City. TENNESSEE Chattanooga Knoxville Memphis. Nashville TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. Galveston Houston. Port Arthur. San Antonio. UTAH Salt Lake City. Vernal | .24 .22 -14 -10 . 7 . 18 . 19 . 18 . 14 . 20 11 .33 .35 .22 . 31 .24 .22 .36 .32 .32 .30 8 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville Memphis Nashville. TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. Galveston Houston. Port Arthur San Antonio. UTAH Sait Lake City. Vernal | .24 .22 -14 -10 .77 .18 .19 .18 .14 .20 11 .33 .39 .35 .22 .31 .30 8 0 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville. TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. Galveston Houston. Port Arthur San Antonio. UTAH Salt Lake City. Vernal VERMONT Burlington. | .24 .22 -14 -10 .77 .18 .19 .18 .14 .20 11 .33 .39 .35 .22 .31 .30 8 0 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville. TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. Galveston Houston. Port Arthur San Antonio UTAH Salt Lake City. Vernal VERMONT Burlington. | .24 .22 -14 -10 .7 .18 .19 .18 .19 .18 .19 .18 .19 .11 .33 .39 .35 .32 .31 .24 .22 .31 .30 8 0 7 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville. TEXAS Abilene. Amarillo. Austin Brownsville. Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. Galveston Houston. Port Arthur San Antonio. UTAH Salt Lake City. Vermal VERMONT Burlington. VIRGINIA Lynchburg | .24 .22 -14 -10 .7 .18 .19 .18 .19 .18 .19 .18 .19 .11 .33 .39 .35 .32 .31 .22 .31 .22 .30 8 0 7 7 |
| Columbia. Greenville SOUTH DAKOTA Huron. Pierre. Rapid City. TENNESSEE Chattanooga Knoxville. Memphis. Nashville. TEXAS Abilene Amarillo. Austin Brownsville. Corpus Christi Dallas. Del Rio. El Paso. Ft. Worth. Galveston Houston. Port Arthur San Antonio UTAH Salt Lake City. Vernal VERMONT Burlington. | .24 .22 -14 -10 .77 .18 .19 .18 .19 .18 .14 .20 11 .33 .35 .32 .31 .24 .22 .31 .24 .22 .31 .24 .22 .31 .30 77 .16 .22 7 |



Weil-McLain 500 Blaine Street Michigan City, Indiana 46360-2388 Customer Service: 800-654-2109

| WASHINGTON |
|----------------------|
| Seattle |
| Spokane2 |
| Yakima5 |
| WEST VIRGINIA |
| Elkins6 |
| Parkersburg |
| WISCONSIN |
| Green Bay9 |
| La Crosse9 |
| Madison7 |
| Milwaukee4 |
| WYOMING |
| Cheyenne |
| Lander11 |
| Sheridan8 |
| |
| CANADA |
| ALBERTA |
| Calgary23 |
| Edmonton25 |
| Grand Prairie |
| McMurray39 |
| BRITISH COLUMBIA |
| Kamloops10 |
| Prince George |
| Vancouver |
| Victoria |
| MANITOBA |
| Churchill |
| Dauphin26 |
| Winnipeg27 |
| NEW BRUNSWICK |
| Edmunston16 |
| Fredericton11 |
| Moncton7 |
| St. John8 |
| NEWFOUNDLAND |
| Gander1 |
| Goose Bay25 |
| St. Johns |
| NOVA SCOTIA |
| Halifax |
| Yarmouth |
| ONTARIO |
| Hamilton 1 |
| Kenora28 |
| London 0 |
| Ottawa13 |
| Sault Ste Marie15 |
| Timmins28 |
| Toronto1 |
| PRINCE EDWARD ISLAND |
| Charlottetown4 |
| QUEBEC |
| Montreal10 |

Montreal -10 Quebec-12 Sept Illes -22 Vald'Or-27 SASKATCHEWAN Prince Albert-35 Regina-29 Saskatoon.....-31 YUKON Whitehorse.....-43

NOTE: These values are the 971/2% figures recommended in energy conservation standards, like ASHRAE 90A-1980. Adjustments may be made to reflect local climates which differ from the tabulated temperatures, or local weather experience.