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## **WEIL-MCLAIN**

SVF 2500-3000 S2 BOILER

DES. J. ROBERSON

**JOB NO.** 11-2315

DATE

7/5/23

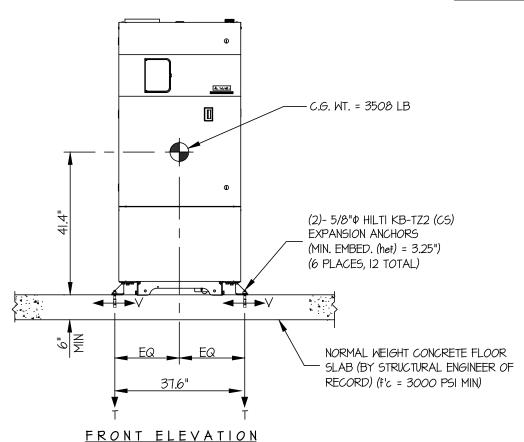
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SHEET

SHEETS

SEISMIC ANCHORAGE

SLAB ON GRADE



Tu = 1889 LB/BOLT (MAX)Vu = 749 LB/BOLT (MAX)

#### NOTES:

1. FORCES ARE DETERMINED PER 2022 CALIFORNIA BUILDING CODE AND ASCE 7-16. STRENGTH DESIGN IS USED. (EXAMPLE: SDS = 2.20,  $\Omega_p$  = 1.0,  $I_p$  = 1.5,  $R_p$  = 2.5,  $\Omega_o$  = 2.0, z/h = 0)

HORIZONTAL FORCE (Eh) = 0.99 Wp

HORIZONTAL FORCE (Emh) = 1.98 Wp (FOR CONCRETE ANCHORAGE)

VERTICAL FORCE (Ev) = 0.44 Wp

- 2. THIS CALCULATION ENCOMPASSES WEIGHTS AND VERTICAL C.G. POSITIONS NOT EXCEEDING VALUES SHOWN.
- 3. THIS CALCULATION WAS PREPARED WITHOUT KNOWLEDGE OF ANY SITE CONDITION. COMPATIBILITY FOR USE WITH A SITE SHALL BE EVALUATED BY THE STRUCTURAL ENGINEER OF RECORD OF THE INSTALLATION (SEOR). USE REQUIRES APPROVAL BY THE SEOR.
- 4. STRUCTURAL ENGINEER OF RECORD FOR THE INSTALLATION SHALL VERIFY ALL CONDITIONS, EVALUATE INTERACTION WITH ADJACENT EQUIPMENT AND ANCHORS, AND PROVIDE SUPPORT STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN IN COMBINATION WITH ALL OTHER LOADS THAT MAY BE PRESENT.



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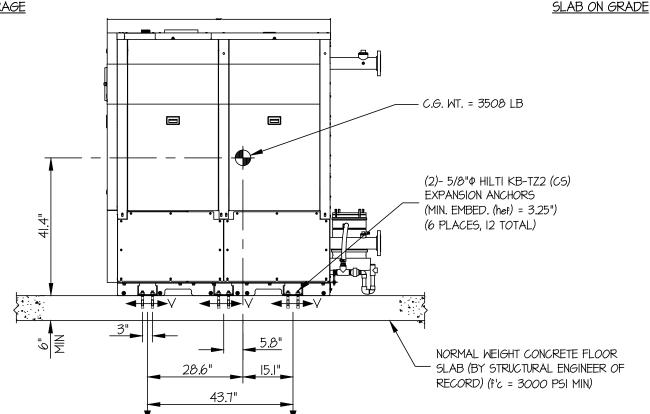
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of **2** sheets

SHEET

SVF/2500-3000 S2 BOILER

SEISMIC ANCHORAGE



#### SIDE ELEVATION

LOADS:

WEIGHT ( $W_p$ ) = 3508 LB

HORIZONTAL FORCE (Emh) = 1.98 Wp = 6946 LB

VERTICAL FORCE (E<sub>v</sub>) = 0.44 W<sub>p</sub> = 1544 LB

ANCHOR SPEC: 5/8" PHILTI KB-TZ2 (CS): (hef = 3.25")

SPACING = 3" MIN

EDGE DISTANCE = 32" MIN:

 $\phi T = 0.75 \phi Nn$  = 2148 LB/ANCHOR (TENSION)

 $\phi V = \phi V n$  = 6169 LB/ANCHOR (SHEAR)

ANCHOR FORCES:

TENSION (T)

SHEAR (V)

Vu maximum = 
$$\begin{bmatrix} 6946\#(28.6") \\ \hline 8 \text{ BOLTS } (43.7") \end{bmatrix} \times (0.3) \end{bmatrix} + \frac{6946\#}{12 \text{ BOLTS}} = 749 \text{ LB/BOLT (MAX)}$$

INTERACTION:

$$\left(\frac{\mathsf{Tu}}{\Phi \mathsf{T}}\right) + \left(\frac{\mathsf{Vu}}{\Phi \mathsf{V}}\right) \quad \leq 12 \quad \left(\frac{1889}{2148}\right) + \left(\frac{749}{6169}\right) = 1.00 \leq 12 \quad \text{°.} \quad \underline{O.K.}$$

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OF

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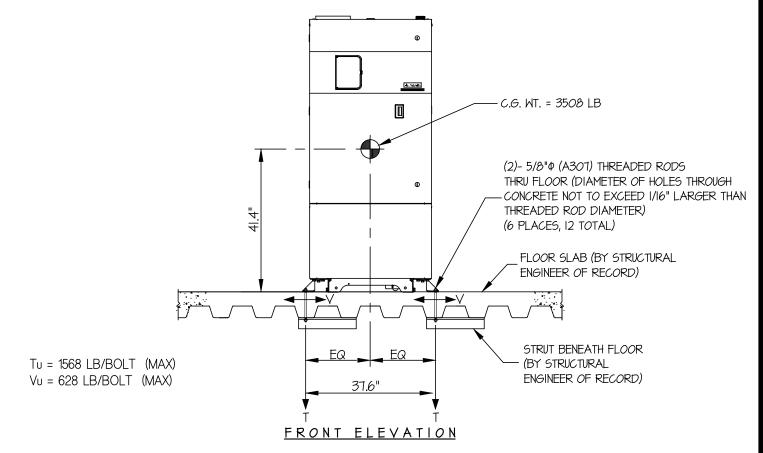
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UPPER FLOOR SEISMIC ANCHORAGE

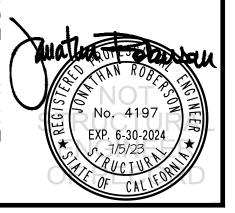


#### NOTES:

 FORCES ARE DETERMINED PER 2022 CALIFORNIA BUILDING CODE AND ASCE 7-16. STRENGTH DESIGN IS USED. (EXAMPLE: SDS = 2.30,  $\Delta p = 1.0$ , |p| = 1.5, Rp = 2.5, z/h < 1)

> HORIZONTAL FORCE (En) = 1.66 WpVERTICAL FORCE (Ev) = 0.46 Wp

- 2. THIS CALCULATION ENCOMPASSES WEIGHTS AND VERTICAL C.G. POSITIONS NOT EXCEEDING VALUES SHOWN.
- 3. THIS CALCULATION WAS PREPARED WITHOUT KNOWLEDGE OF ANY SITE CONDITION, COMPATIBILITY FOR USE WITH A SITE SHALL BE EVALUATED BY THE STRUCTURAL ENGINEER OF RECORD OF THE INSTALLATION (SEOR), USE REQUIRES APPROVAL BY THE SEOR.
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SHEETS

OF SEISMIC ANCHORAGE UPPER FLOOR – C.G. WT. = 3508 LB (2)- 5/8" (A307) THREADED RODS THRU FLOOR (DIAMETER OF HOLES THROUGH CONCRETE NOT TO EXCEED I/I6" LARGER THAN THREADED ROD DIAMETER) (6 PLACES, I2 TOTAL) FLOOR SLAB (BY STRUCTURAL ENGINEER OF RECORD) 5.8" STRUT BENEATH FLOOR 28.6" 15.1". (BY STRUCTURAL ENGINEER OF RECORD) 43.7"

#### SIDE ELEVATION

LOADS:

WEIGHT (Wp) = 3508 LB

HORIZONTAL FORCE (Eh) = 1.66 Wp = 5823 LB

VERTICAL FORCE (Ev) = 0.46 Wp = 1614 LB ANCHOR SPECS: 5/8"\$ (A307) THREADED ROD

φT= 9870 LB/BOLT (TENSION)

φV= 5890 LB/BOLT (SHEAR)

#### ANCHOR FORCES:

TENSION (T)

Tu maximum = 
$$\left[\frac{5823\#(41.4'')(28.6'')}{4 \text{ Bolts }(37.6'')(43.7'')} \times (0.3)\right] + \frac{5823\#(41.4'')}{4 \text{ Bolts }(43.7'')} - \frac{(3508\#(0.9) - 1614\#)(28.6'')}{8 \text{ Bolts }(43.7'')} = 1568 \text{ LB/BOLT (MAX)}$$

(HORIZ - FRONT TO BACK) (HORIZ - SIDE TO SIDE) (WEIGHTI(0.9) - E<sub>V</sub>)

SHEAR (V)

Vu maximum = 
$$\left[ \frac{5823\#(28.6'')}{8 \text{ Bolts } (43.7'')} \times (0.3) \right] + \frac{5823\#}{12 \text{ Bolts}} = 628 \text{ LB/BOLT (MAX)}$$

# EASE

#### **EQUIPMENT ANCHORAGE & SEISMIC ENGINEERING**

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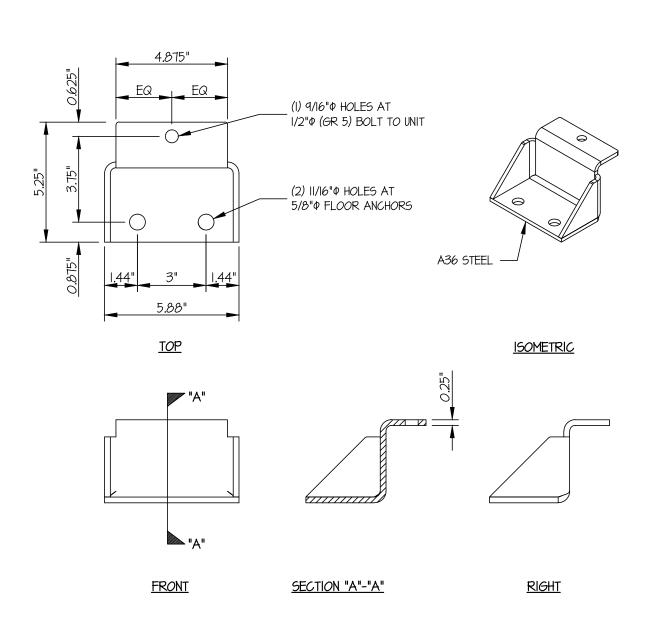
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SEISMIC ANCHORAGE

BRACKET DETAILS



FLOOR ANCHOR BRACKET